

# Application Advantages of Monolithic Fully Signal Conditioned Pressure Sensors

### **▲WARNING**

#### **MISUSE OF DOCUMENTATION**

- The information presented in this application sheet is for reference only. Do not use this document as product installation information.
- Complete installation, operation, and maintenance information is provided in the instructions supplied with each product.

**Failure to comply with these instructions could result in death or serious injury.**

### **INTRODUCTION**

Fully signal conditioned single chip pressure sensors are available in ranges from 1 psi to 500 psi and offer several advantages over discrete sensors with interface electronics. These devices have good to excellent linearity and are fully interchangeable within the set pressure range. They have a standard form factor and solderable ports. System designers realize many advantages when using the monolithic fully signal conditioned pressure sensors for new applications.

### **BACKGROUND**

Honeywell has developed a family of silicon based piezoresistive single chip fully signal conditioned pressure sensors. These sensors provide high accuracy, wide operating temperature range, high reliability, and small package outline. These sensors are available for a relatively low cost.

It is important to define the parameters necessary to describe a pressure sensor. The ideal transfer function for a pressure sensor is:

Equation 1.

$$V_{out} = S_n * P + N$$

Where  $S_n$  is the sensitivity and  $N$  is the null set point. The transfer function is specified for a referenced supply voltage.

Parameters of interest for high accuracy sensor designs are: linearity, ratiometricity, stability, repeatability, hysteresis, null set point, span set point, null temperature shift and span temperature shift. However, accuracy specifications vary widely among manufacturers.

### **MAPPING SENSOR ACCURACY**

When determining the accuracy of a pressure sensor, the most meaningful performance parameter is a total error specification over the entire operating range. The response map in Figures 1 and 2 (see page 2) shows, in a single picture, the total error over the entire operating range of pressure and temperature from all sources of error except ratiometricity. The z-axis is the output voltage deviation from an ideal sensor as a percentage of a full scale output. The y-axis is temperature in degrees Celsius. The x-axis is pressure. Figure 1 shows a 3D surface map of a typical monolithic 15 psi sensor. Figure 2 shows a 3D surface map of a typical temperature compensated discrete 15 psi sensor.

Figure 1 shows that the accuracy of the monolithic devices makes them easily interchangeable. This means the system user does not have to be concerned with calibration. If auto-zero can be used, the measurement becomes virtually error free. Monolithic fully signal conditioned devices have in-package laser trimming after characterization over temperature to adjust the offset, sensitivity, offset temperature compensation (TC) and sensitivity TC. As shown in Figure 1, this device achieves a 1% or less error over the response surface for a temperature range of  $-40^{\circ}\text{C}$  to  $125^{\circ}\text{C}$ .

Figure 2 shows that temperature compensation for a discrete device is limited to about  $0^{\circ}\text{C}$  to  $85^{\circ}\text{C}$ . Discrete devices are typically compensated using series compensation. In this process, trimmable resistors, in series with the bridge, are positioned between both supply and ground. This compensation method relies on the relationship between the bridge resistors' TC and the bridge sensitivity TC being closely matched in opposite directions. Referring to Equation 1, the term  $S_n$  has the following relationship:

Equation 2.

$$S_n(t) = S_n(o) (1 + \alpha T + \beta T^2) V_b(t) / V_b(o)$$

As can be seen from Equation 2, if the TC of sensitivity,

$$(S_n(t))$$

Figure 1. Monolithic Sensor Response Map

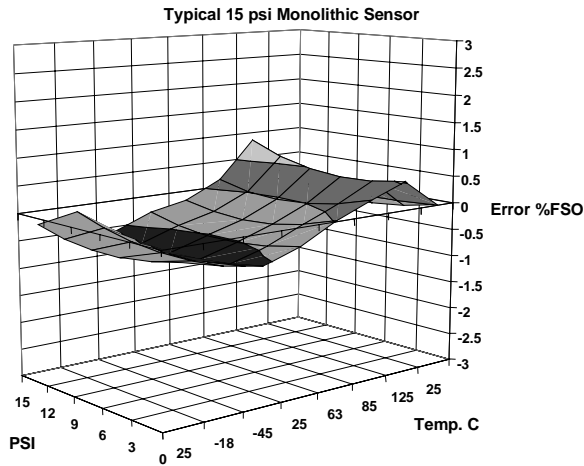
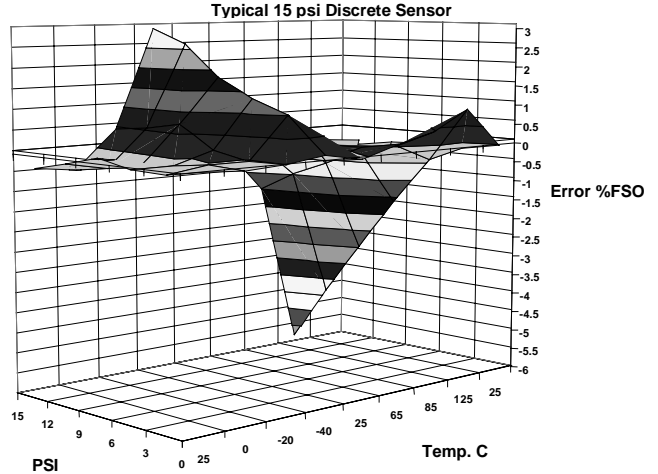


Figure 2. Discrete Sensor Response Map



is negative and the TC of the bridge voltage,

$$((1 + \alpha T + \beta T^2)V_b(t))$$

is positive, the device can be designed to allow trimming the sensitivity TC.

Discrete sensors are sold as either uncompensated or compensated devices. Uncompensated sensors have a range of offsets and sensitivities based on the diaphragm dimensions and manufacturing process variations. These devices do not have temperature compensation. These sensors can not be used for applications requiring a total error accuracy of less than 10% without sophisticated external circuitry and test equipment to characterize each device.

Compensated devices have the null, sensitivity and sensitivity TC adjusted by thin film laser trimming. These sensors have a tighter error band than uncompensated devices. As seen in Figure 2, this type of compensation produces a 3% or less error over the response surface for a temperature range of 0°C to 85°C. Offset temperature compensation requires characterization over temperature to determine the proper compensation. Temperatures above 85°C or below 0°C quickly degrade the accuracy of compensated discrete devices.

### DESIGNING FOR ACCURACY

Linearity, stability, hysteresis, ratiometricity, and repeatability are critical design parameters for high accuracy sensors. Diaphragm design begins with specifying the diaphragm sensitivity, linearity, and burst pressure requirements. The diaphragm side length sets the die size. These parameters require careful consideration: the sensitivity of the die is a

function of the diaphragm side length to thickness given by the following:

Equation 3.

$$V_{out} = K * V_{bridge} * P * (L/T)^2$$

Linearity is a fourth order effect of the ratio of diaphragm side length to thickness and the pressure range given by the following:

Equation 4.

$$TBL = K * P * (L/T)^4$$

The burst pressure is related to the edge stress on the diaphragm and is given by the following:

Equation 5.

$$Stress = K * P * (L/T)^2$$

In Equations 4 and 5, K is a constant but is not the same value in each equation. P is pressure, while L and T represent the diaphragm length and thickness. As can be seen from Equations 3, 4, and 5, the larger and thinner the diaphragm, the more sensitive it becomes. However, linearity and burst pressure are degraded. In addition, for larger diaphragms, the die size and cost are increased.

Ratiometricity, stability, repeatability, and thermal hysteresis involve manufacturing process considerations, as does the mechanical interface used for mounting the silicon to the port. The mechanical properties of silicon provide a highly reliable diaphragm that tolerates burst pressures

several times the operating pressure. The device has virtually no mechanical hysteresis when properly designed. Hysteresis for these devices is dominated by thermal incompatibilities between the silicon and the mounting materials. Monolithic sensor electronics are designed to be ratiometric and laser trimmed.

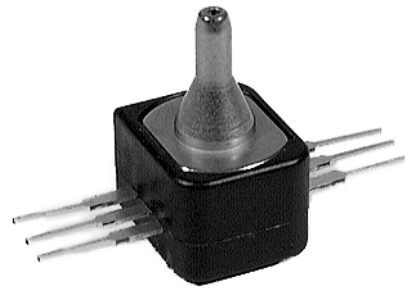
Supply voltage is also a consideration when selecting a ratiometric sensor. Discrete sensors have different nominal supply voltages over which their typical operation is specified. Usually this is to provide a desired sensitivity. Depending on the device, this may be 8 V, 10 V or even 12 V. Discrete sensors have differential output voltages of up to 100 mV. The requirement for full scale output of the diaphragm is related to the signal-to-noise ratio of the system. Because the output signals from the bridge must be routed for use, sufficient signal levels must be maintained for signal integrity.

The monolithic sensor is specified at a 5 V supply with a linear output from 0.5 V to 4.5 V. Integrated amplification of the bridge signal produces a sensor with high accuracy as measured with respect to the full scale output. Thus, the full scale output has been increased by an order of magnitude from millivolts to volts. With discrete sensors, amplification is required to interface the signal to a controller.

The monolithic sensor, shown in Figure 3, is built in a 6 pin DIP package that is easily mounted to a PC board. This small size optimizes PC board space. The port design is compatible with an O-ring interface that allows overpackaging if the system requires.

The sensor construction is highly reliable and offers excellent media compatibility. Standard silicon integrated circuit fabrication techniques are used to produce the die that is bonded to a glass stress isolation structure. This component is then solder mounted to the port to provide media compatibility with air, water, engine fuel, oil and transmission fluids.

System cost is always a trade off. Designers must achieve the required performance with a product that will provide a reasonable return. System designers look for components that will reduce manufacturing costs without compromising system performance. Although the price of a single chip fully compensated sensor is somewhat higher than a discrete sensor, Figure 3. Monolithic Pressure Sensor



the single chip solution is more cost effective when the entire system is considered.

## SUMMARY

The monolithic fully signal conditioned sensor offers many advantages when used in applications. The single chip fully compensated sensor is packaged in a 6-pin DIP that provides a small package outline that can be mounted directly to a PC board. This eliminates the cost associated with mounting brackets. The sensors operate from a 5 V supply and have a linear output from 0.5 V to 4.5 V providing a direct interface to an A/D input on a controller. Unlike discrete devices, the monolithic sensor requires no additional interface circuitry to perform the output signal function. This saves cost in several ways. Design time is saved by eliminating the interface electronics as well as simplifying the PC board design. The cost of the interface electronics is eliminated. Calibration over temperature can be very costly when attempting to match the performance of discrete and single chip devices. Conservation of board space is achieved with the use of a single component. This also reduces cost. Procurement costs are higher with a system that uses a discrete sensor with interface electronics as opposed to one that uses a single component.

Overall, a system designer should consider the total system cost by comparing the cost of the single chip fully compensated sensor with the cost of the discrete sensor with interface electronics to achieve the desired total error band.

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